

LIMITS OF SEPARATION PERFORMANCE IN SFC

SHIMADZU SFC USER MEETING

Ken Broeckhoven

**Department of Chemical Engineering (CHIS)
Vrije Universiteit Brussel (VUB), Belgium**

ADVANTAGES OF SFC

- Supercritical Fluid Chromatography/SFC (incl. sub-critical conditions) employs a low viscosity mobile phase that contains mainly CO₂
 - ➔ Viscosity η between 0.1-0.25 cP for 10-50% MeOH at 30°C and 150 bar (vs. 0.8 cP for water at 30°C) (1 cP = 1mPa·s)
 - ➔ Fast separations possible: high $D_{\text{mol}} \sim 1/\eta$
 - Optimal velocity $u_{\text{opt}} \sim D_{\text{mol}}$
 - Fast mass transfer: C-term $\sim 1/D_{\text{mol}}$
 - ➔ Low column pressure drop since $\Delta P \sim \eta$ (but also $\sim u_{\text{opt}}$)
- “Green” technique (low waste/solvent use), unique selectivity and orthogonality, chiral separations, advantages for scale up to prep...

ADVANTAGES OF SFC

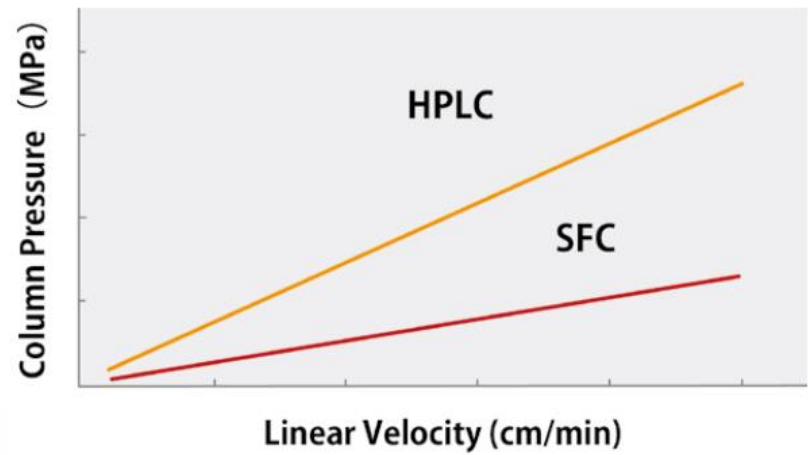


Fig. 8 Linear Velocity vs. Column Back Pressure

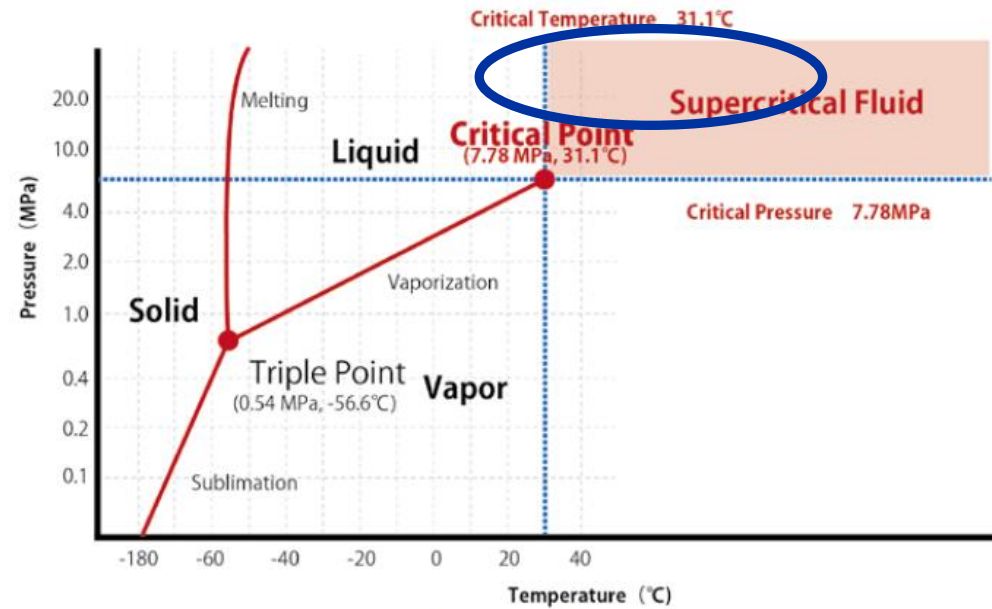
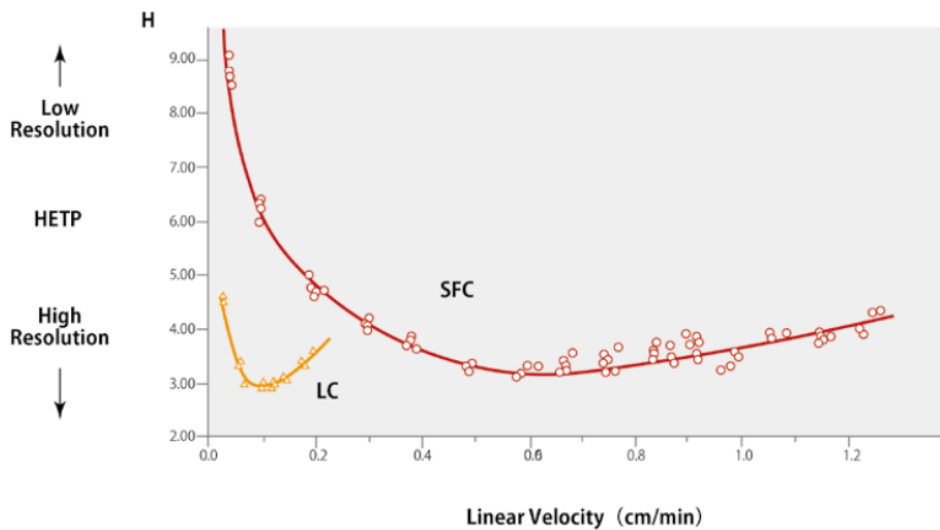


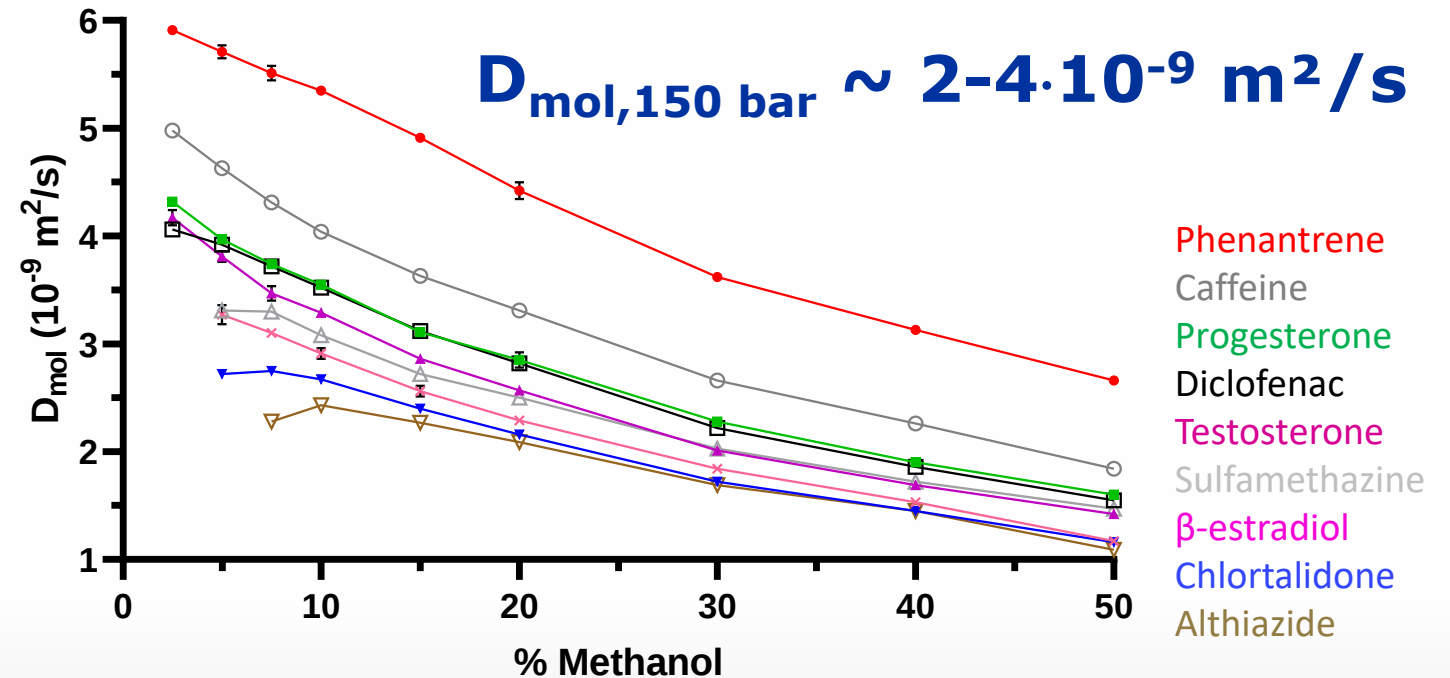
Fig. 1 Phase Diagram for Carbon Dioxide

Table 1 Physical Properties of Supercritical Fluids

	Diffusion Coefficient (m ² /s)	Density (g/cm ³)	Viscosity (g/cm·s)
Liquids	10 ⁻⁶	1	10 ⁻²
Supercritical Fluids	10 ⁻³	0.2-0.8	10 ⁻³
Gases	10 ⁻¹	10 ⁻³	10 ⁻⁴

ADVANTAGES OF SFC

- Diffusion coefficients in SFC claimed to be very high (10^{-7} - 10^{-8} m²/s) relative to LC (10^{-9} m²/s)
- Range of D_{mol} based on small neutral molecules in pure CO₂ at low backpressure (< 100 bar)
- Addition of minor amounts of co-solvent strongly decrease D_{mol}



ADVANTAGES OF SFC

- Density ρ of SFC mobile phases similar or higher than that of modifier
- Density of neat CO_2 exceeds that of methanol above 160 bar

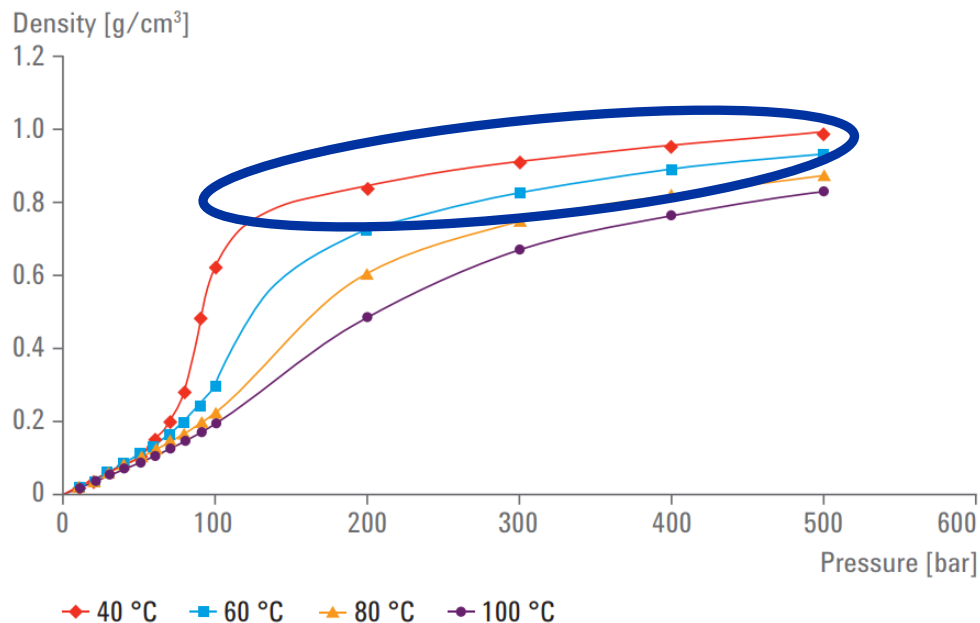
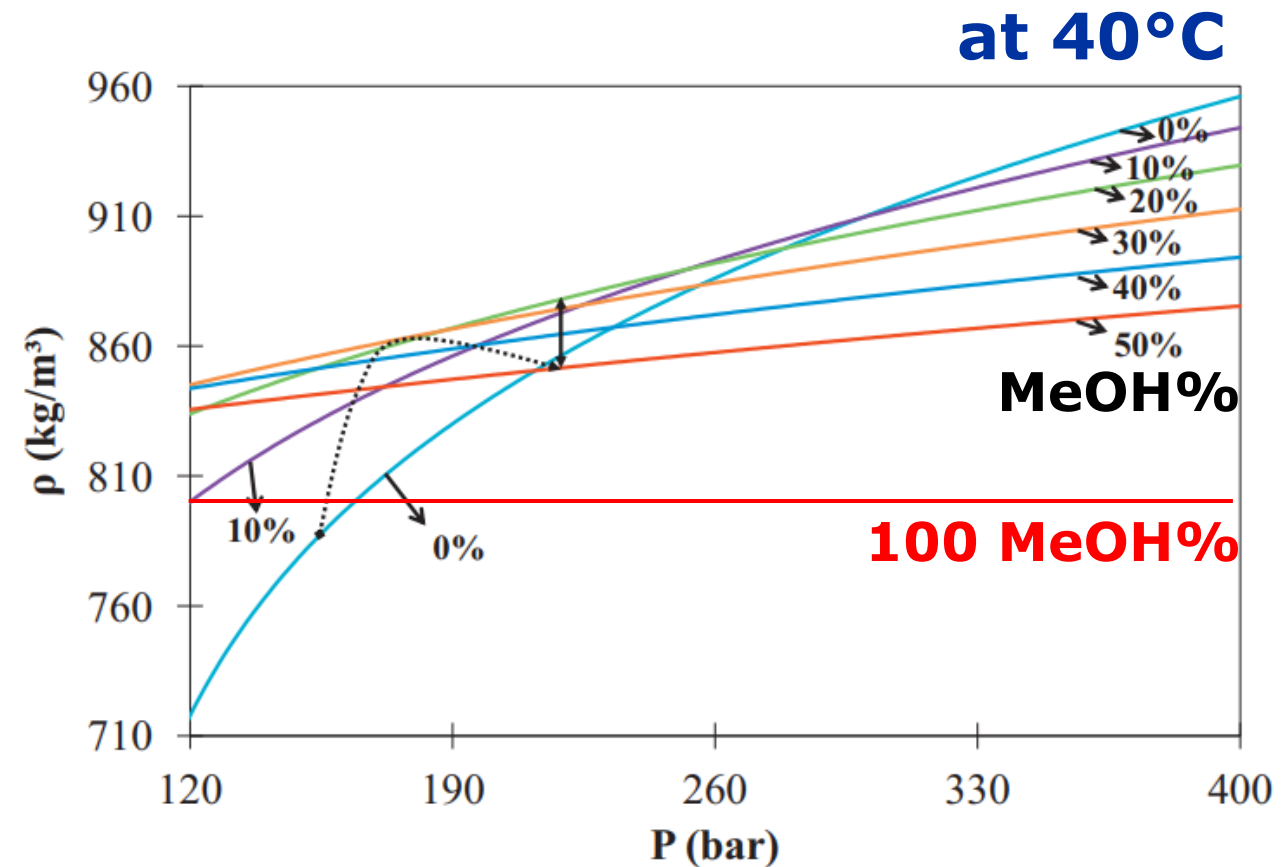
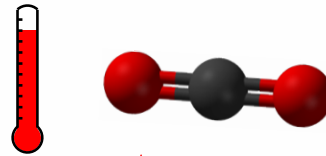
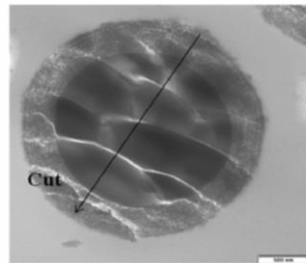


Figure 2.1 Density of pure CO_2 as a function of pressure at four different temperatures. From top to bottom: 40, 60, 80 and 100 °C.



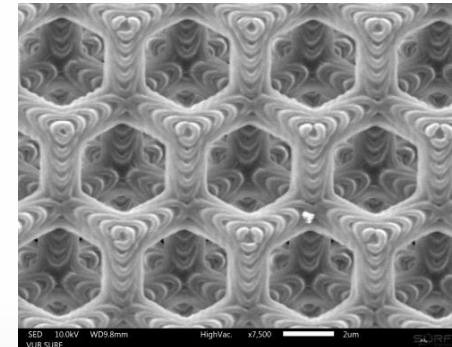
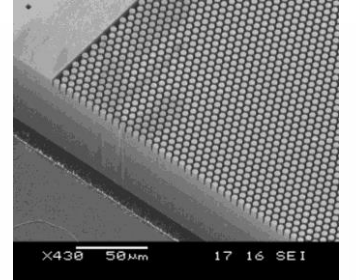
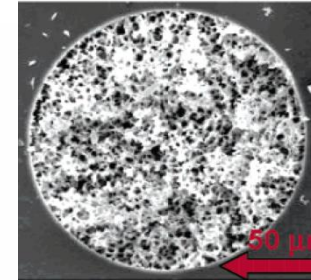
LIMITS OF SEPARATION POWER IN CHROMATOGRAPHY

- Time-efficiency trade off is given by the Knox-Saleem equation for a fully optimized system (flow rate, particle size and column length)
- “Money-equation”:
 - higher separation efficiency N is valuable/expensive
 - time t = money



$$t_0 = \frac{h_{\min}^2 \cdot \eta \cdot \phi}{\Delta P} \cdot N^2$$

HPLC → UHPLC



LIMITS OF SEPARATION POWER: LC VS. SFC

- SFC: same columns as in LC ($h_{\min}$ and ϕ)
- Viscosity is 3-8x lower in SFC than LC
- What about pressure drop?

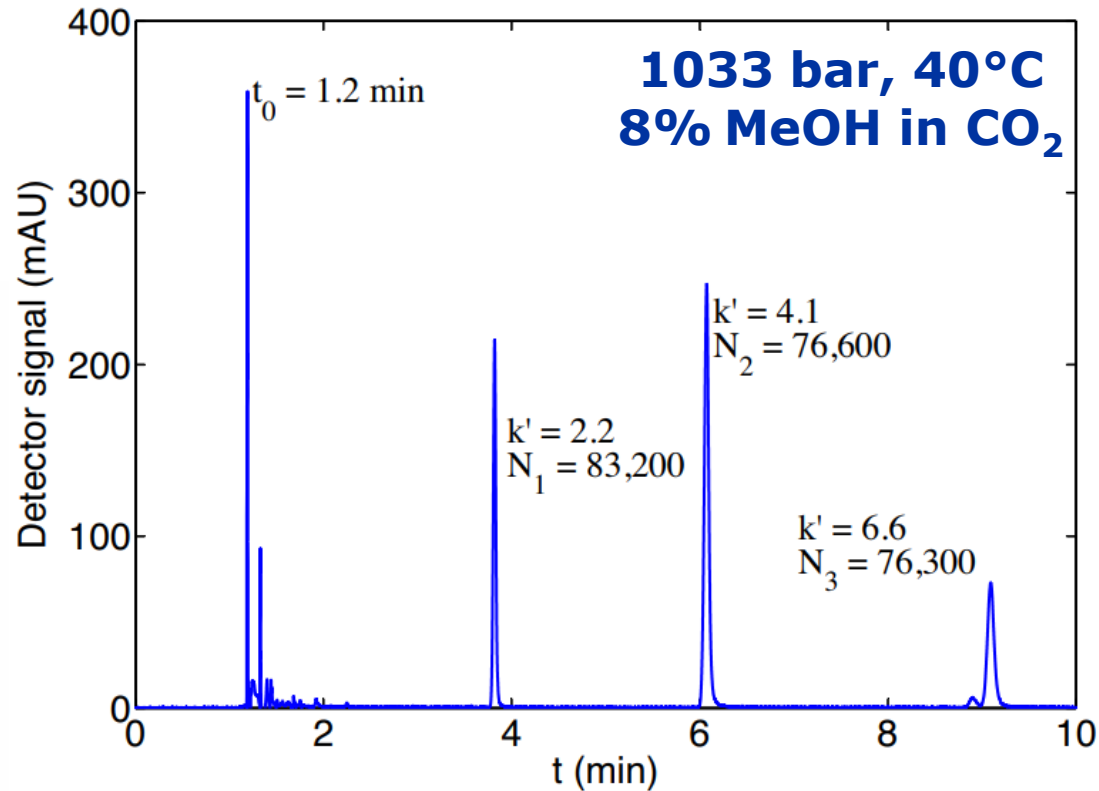
$$t_0 = \frac{h_{\min}^2 \cdot \eta \cdot \phi}{\Delta P} \cdot N^2$$

Mode	$P_{\max}$ (bar)	F (ml/min)
LC	1300-1500	2-5
SFC	413-660	3-5

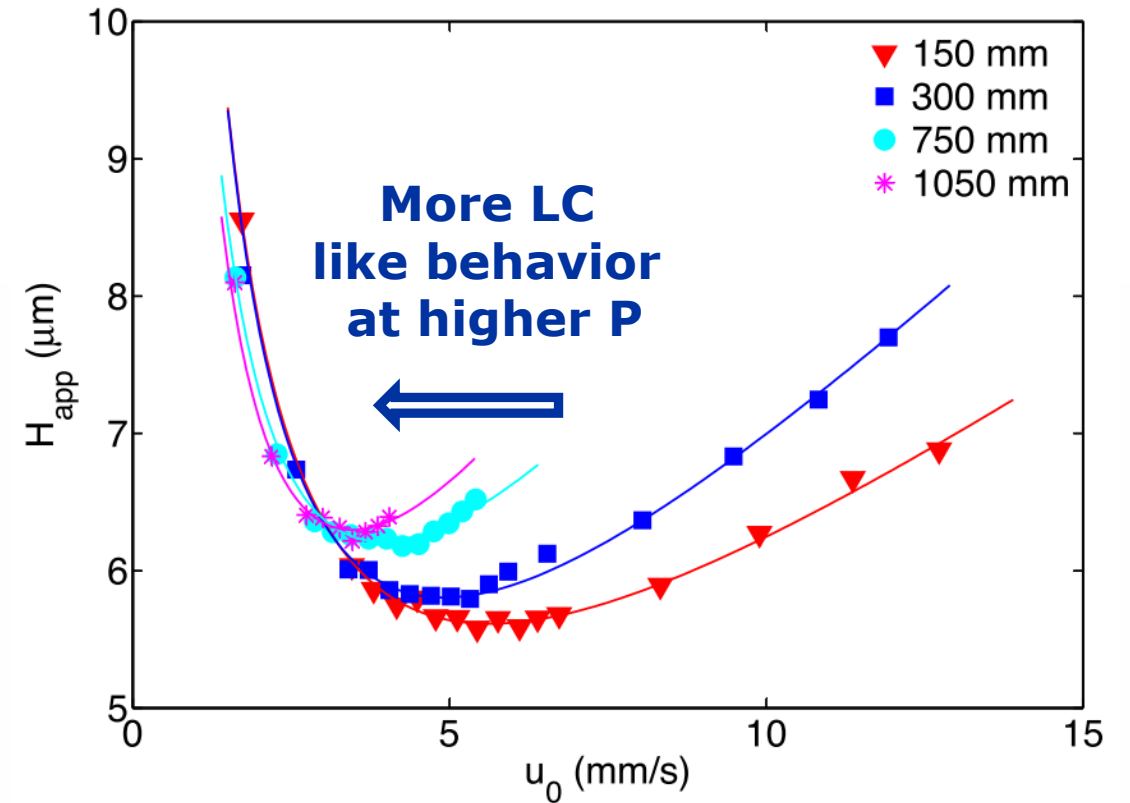
- SFC allows fast separations at low pressure drops, but has similar kinetic performance limits than UHPLC

LIMITS OF SEPARATION POWER FOR SFC

- Is there a fundamental limitation on operating pressure in SFC?



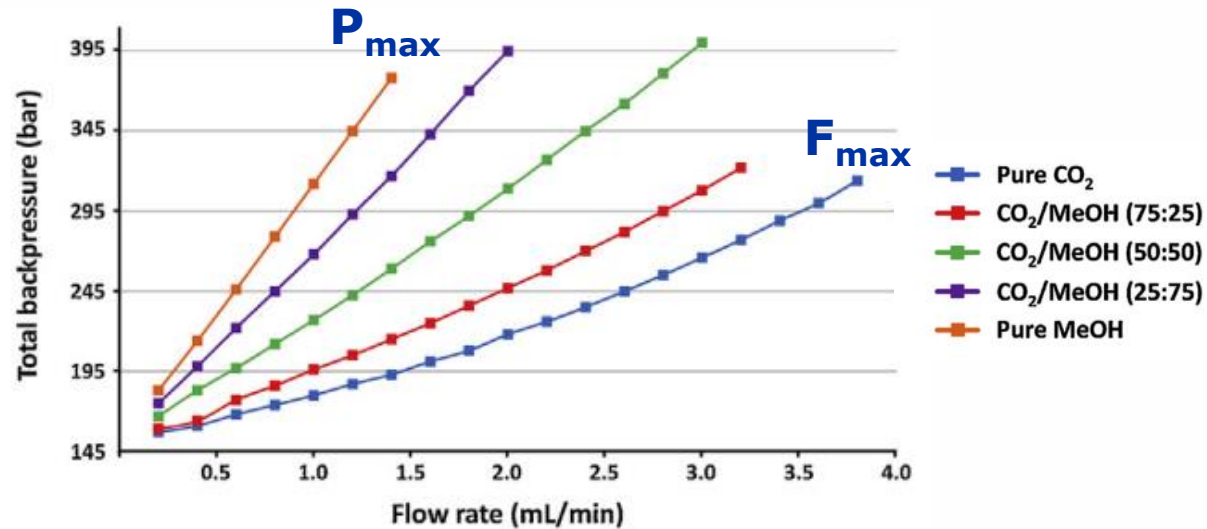
50cm, 2.1mm ID, 1.8 μ m at 1.3mL/min



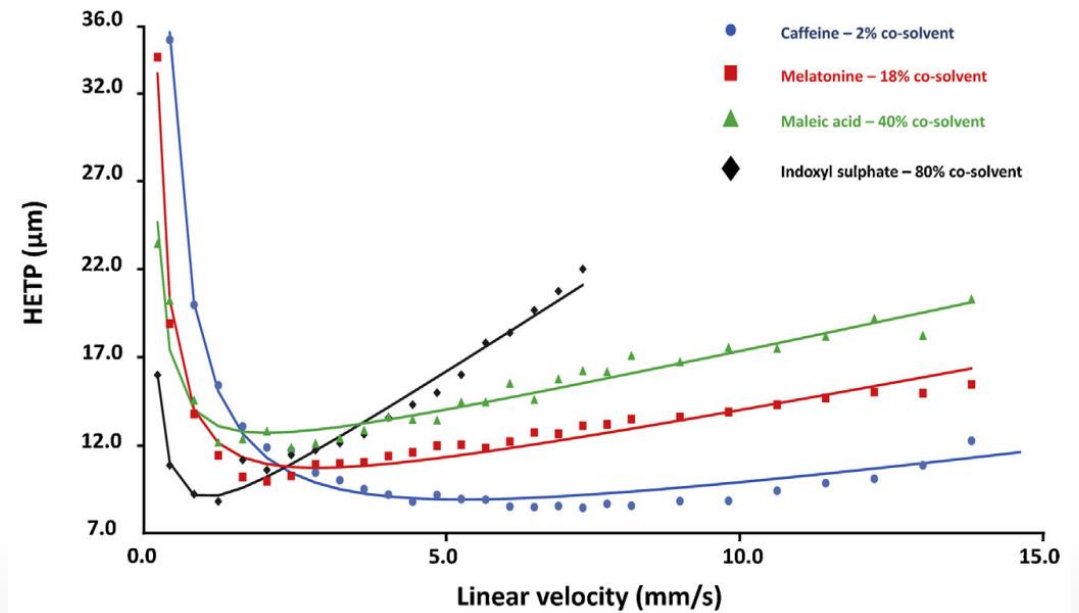
2.7 μ m poroshell, 3mm ID

LIMITS OF SEPARATION POWER FOR SFC

- Bamba and co-workers in 2014 proposed wide elution gradients: SFC => EFLC => HPLC, i.e. from CO₂ to MeOH
- Elution of a wide range of analytes: least to most polar
- Referred to as “unified chromatography” (UC)



Nucleoshell HILIC 2.7 μ m, 100 $\times$ 3.0 mm column



LIMITS OF SEPARATION POWER FOR SFC

- West and co-workers applied combined flow rate and backpressure gradients:

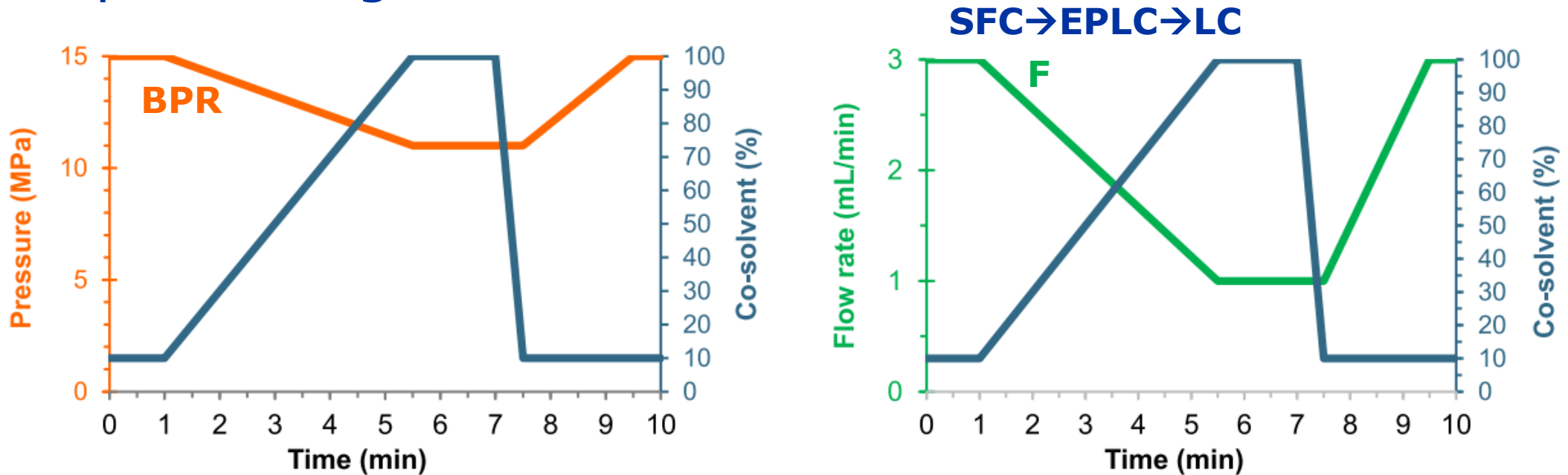
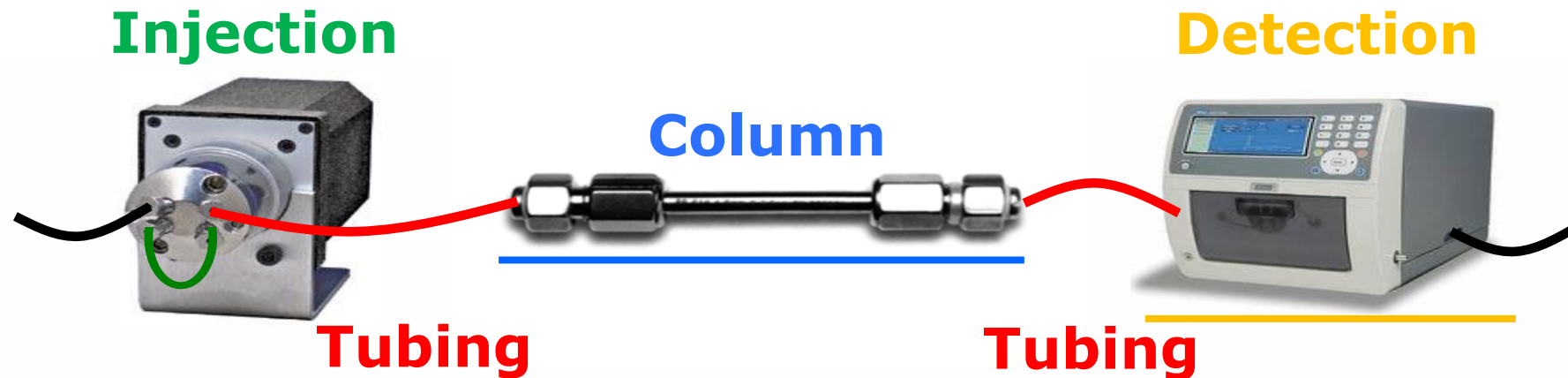


Fig. 1. Gradient profile in the optimized method showing the variation of co-solvent (blue lines), back-pressure (orange lines) and flow rate (green lines).

Chiralpak ZWIX(+), 150 × 3.0 mm, 3 μm

EXTRA-COLUMN BAND BROADENING

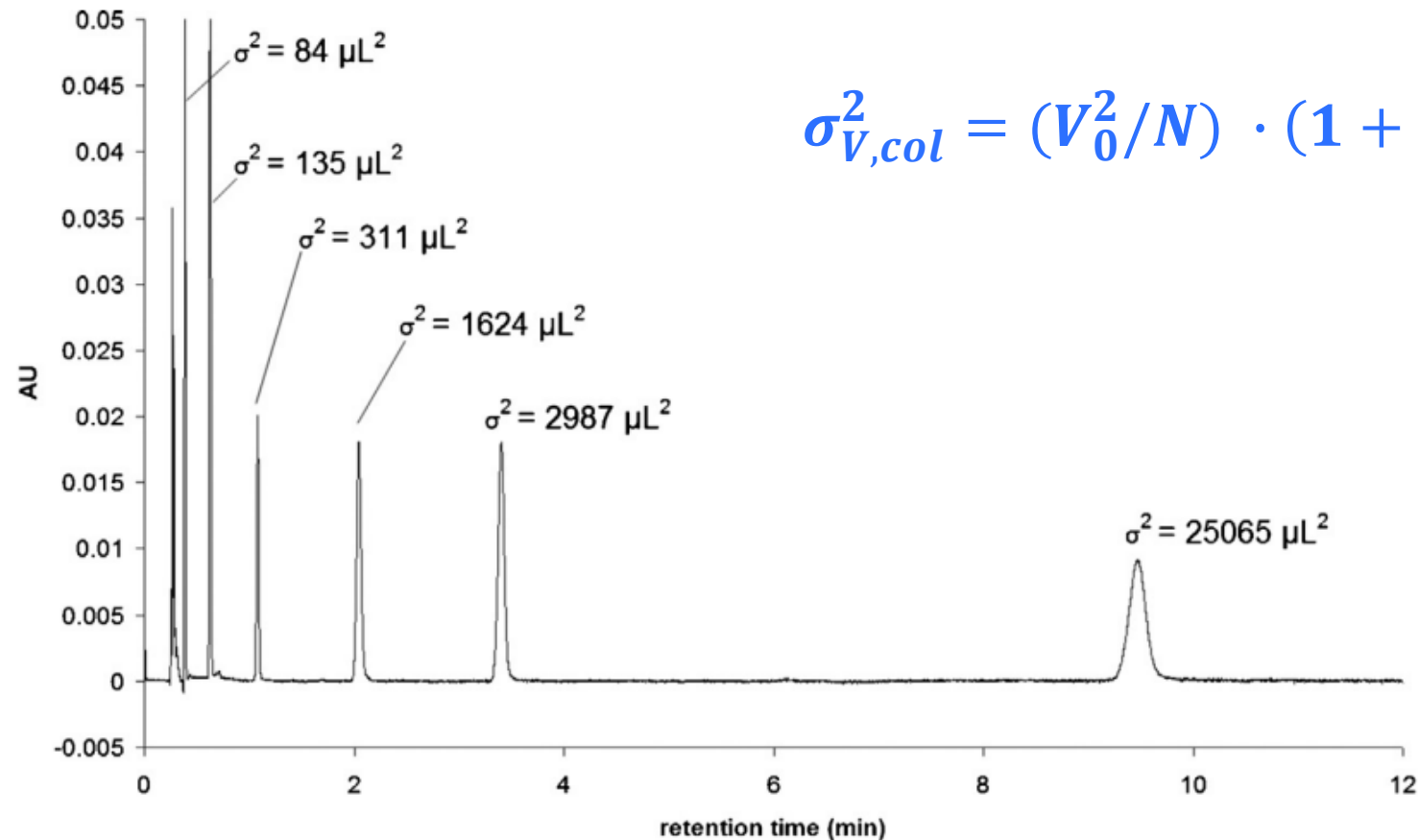
- Separation performance not only determined by mobile phase viscosity, columns and pump pressure
- Instrumental contributions to dispersion and pressure drop:



$$\sigma_{V,tot}^2 = \underbrace{\sigma_{V,inj}^2}_{\text{green}} + \underbrace{\sigma_{V,col}^2}_{\text{blue}} + \underbrace{\sigma_{V,tub}^2}_{\text{red}} + \underbrace{\sigma_{V,det}^2}_{\text{yellow}}$$

$$\sigma_{V,col}^2 = (V_0^2/N) \cdot (1 + k_e)^2$$

EXTRA-COLUMN BAND BROADENING



$$\sigma_{V,col}^2 = (V_0^2/N) \cdot (1 + k_e)^2$$

Fig. 1. Representative chromatogram and peak variances for the estimation of system variance by using the “in presence of column” methodology. Instrument: Acquity UPC², column: Waters BEH 1.7 μm (100 mm $\times$ 3.0 mm) mobile phase: 10% MeOH in CO₂, temperature: 40°C, flow rate: 2 mL/min. Test analytes: butylparaben, caffeine, theobromine, betamethazone, chlorthalidone and hydrochlorothiazide.

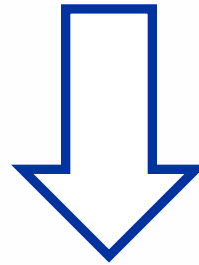
$$\sigma_{V,col}^2 = (V_0^2/N) \cdot (1 + k_e)^2$$

- How large is column dispersion: ($k_e = 2.16$)
 - 4.6mm ID, 25cm, 5 μ m: 2500 μ L²
 - 4.6mm ID, 15cm, 3.5 μ m: 1000 μ L²
 - 2.1mm ID, 10cm, 2 μ m fully porous: 17 μ L²
 - 2.1mm ID, 5cm, 1.5 μ m superficially porous particles: 6 μ L²
- Evolution in extra-column dispersion in LC
 - HPLC systems: 20-100 μ L²
 - UHPLC systems: < 10 μ L², optimized systems < 2 μ L²
- Extra-column dispersion in SFC ?

$$\sigma_{V,col}^2 = (V_0^2/N) \cdot (1 + k_e)^2$$

- Extra-column dispersion in SFC
 - Much less investigated than in LC
 - Estimated by Guillaume and co-workers (10% MeOH in CO₂)
 - 23 and 83 μL^2 for $F = 1\text{ml/min}$ and 2ml/min on UPC²
 - 55 and 81 μL^2 for $F = 1\text{ml/min}$ and 2ml/min on Agilent SFC

$$\sigma_{V,tot}^2 = \sigma_{V,ec}^2 + \sigma_{V,col}^2$$

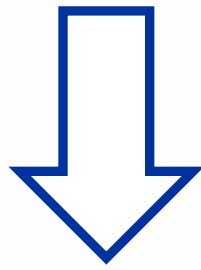


$$N_{obs} = (V_0^2/\sigma_{V,tot}^2) \cdot (1 + k_e)^2$$

EXTRA-COLUMN BAND BROADENING

- Extra-column dispersion in SFC

- 50 μL^2 extra-column dispersion for columns of 15cm long, with $N = 25000$, as a function of k_e for different column ID's
- Observed efficiency

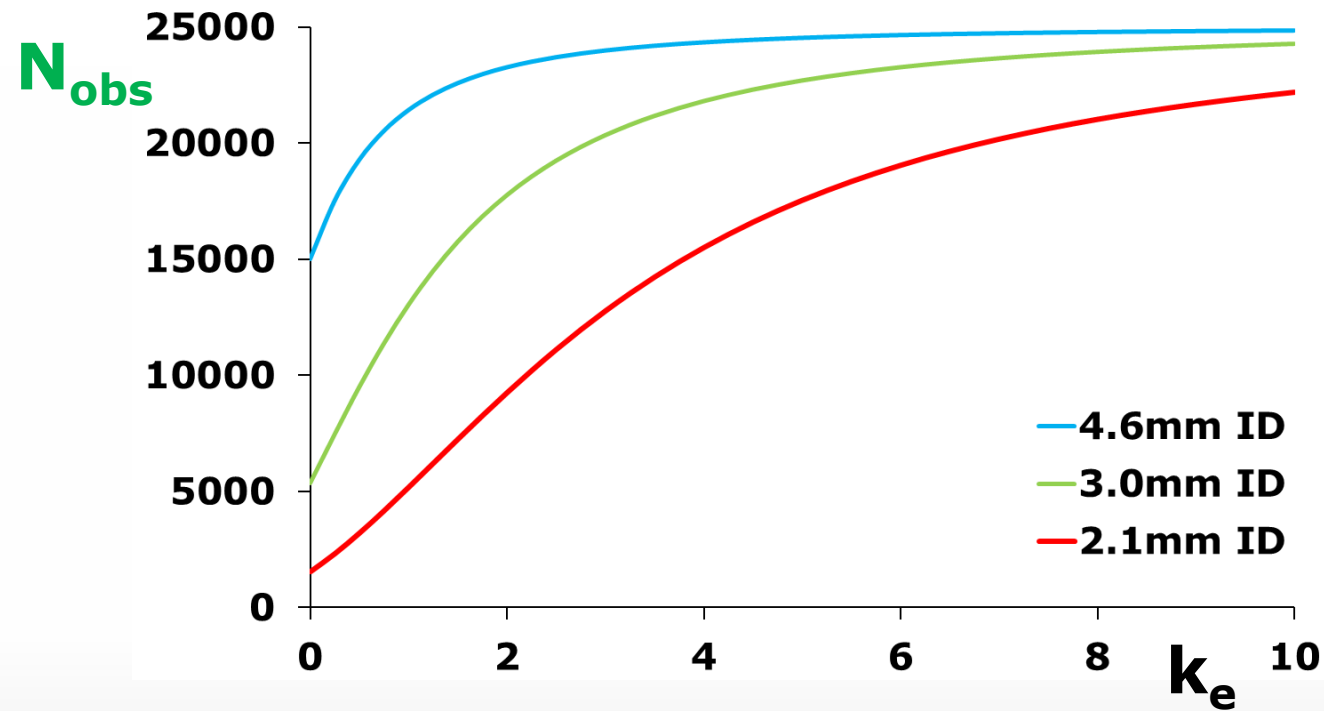


3.0 mm ID trade-off between ECBB and flow rate limitations

$$\sigma_{V,col}^2 = (V_0^2/N) \cdot (1 + k_e)^2$$

$$\sigma_{V,tot}^2 = \sigma_{V,ec}^2 + \sigma_{V,col}^2$$

$$N_{obs} = (V_0^2/\sigma_{V,tot}^2) \cdot (1 + k_e)^2$$



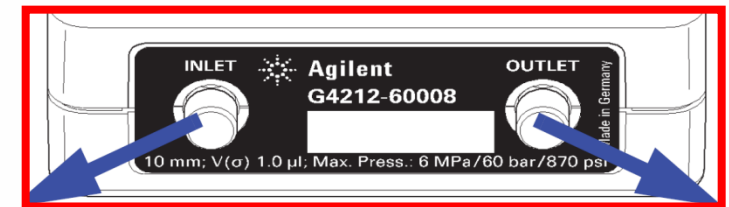
EXTRA-COLUMN BAND BROADENING

- Sources of extra-column dispersion in SFC
 - Analytes are dissolved in a strong(er) solvent (~mainly organic) than mobile phase (~ mainly CO₂)
 - Detector cells design and volumes not optimized as in UHPLC
 - Often larger ID tubing employed (170µm vs. 75-120µm in UHPLC)

EXTRA-COLUMN BAND BROADENING

- Sources of extra-column dispersion in SFC: **detector**
 - Detector contribution: SFC 1.7 μL flow cell vs. ultra-low dispersion max light cartridge

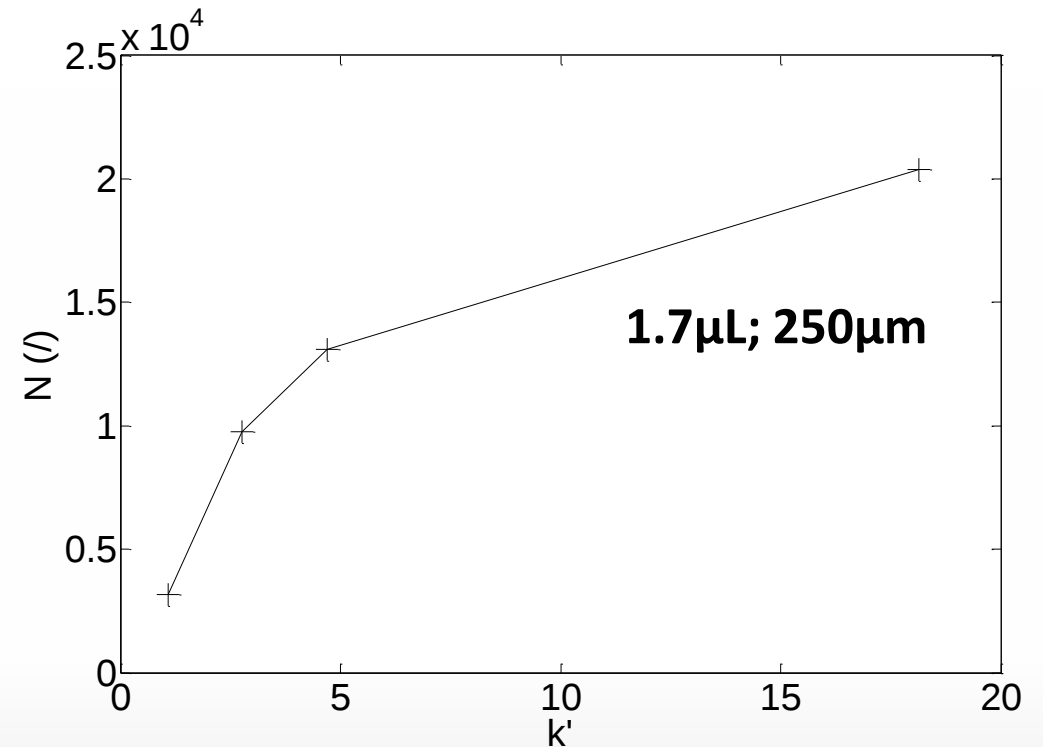
Agilent 1290 Ultra-Low Dispersion
Max-Light Cartridge Flow Cell;
 $V(\sigma)=0.6\mu\text{L}$



Max. Press.: 6 MPa/60 bar/870 psi

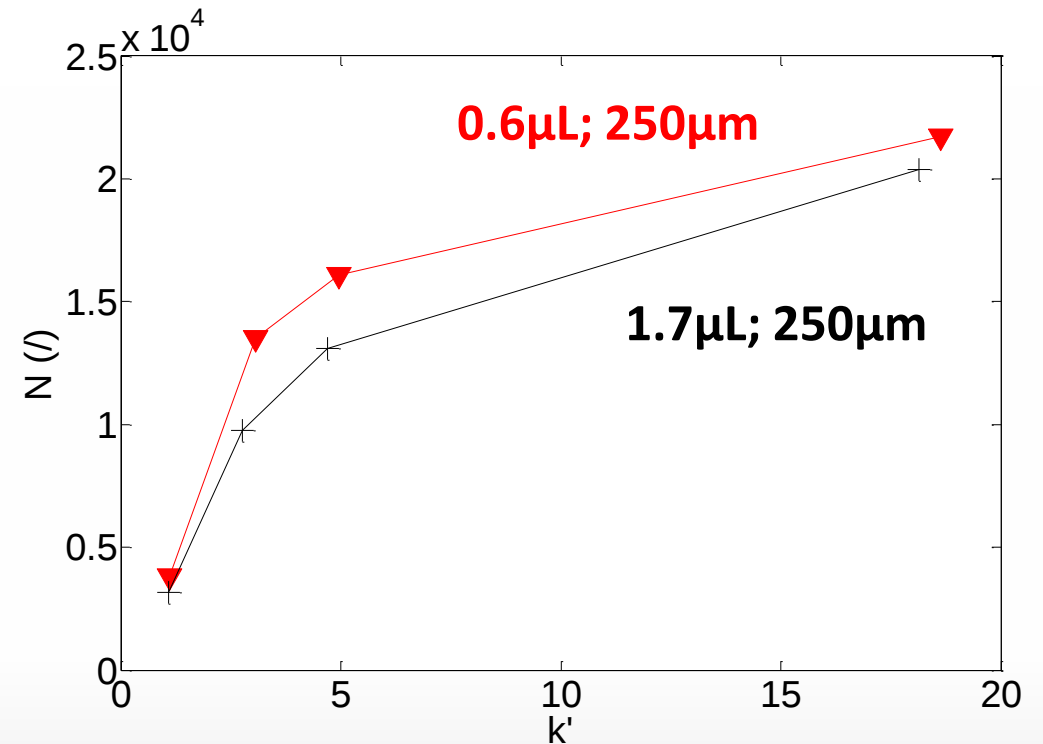
EXTRA-COLUMN BAND BROADENING

- Sources of extra-column dispersion in SFC: **detector**
 - Sample solvent EtOH/IPA/hexane: 10/5/85, $V_{inj} = 0.8\mu\text{L}$
 - $P_{back} = 130$ bar, $2.1 \times 100\text{mm}$ $1.8\mu\text{m}$, $F=1\text{ml/min}$, 8 V% MeOH
 - Tubing
 - Length (50cm)
 - Inner diameter $250\mu\text{m}$ ID



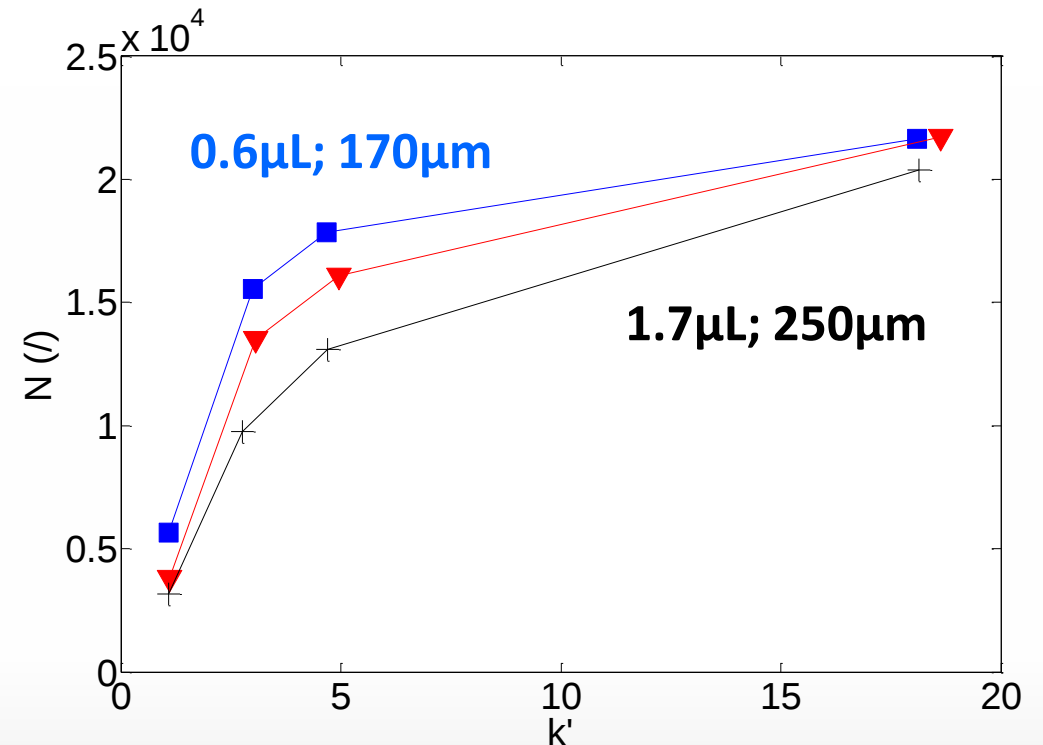
EXTRA-COLUMN BAND BROADENING

- Sources of extra-column dispersion in SFC: **detector**
 - Sample solvent EtOH/IPA/hexane: 10/5/85, $V_{inj} = 0.8\mu\text{L}$
 - $P_{back} = 130$ bar, $2.1 \times 100\text{mm}$ $1.8\mu\text{m}$, $F = 1\text{ml/min}$, 8 V% MeOH
 - Tubing
 - Length (50cm)
 - Inner diameter $250\mu\text{m}$ ID



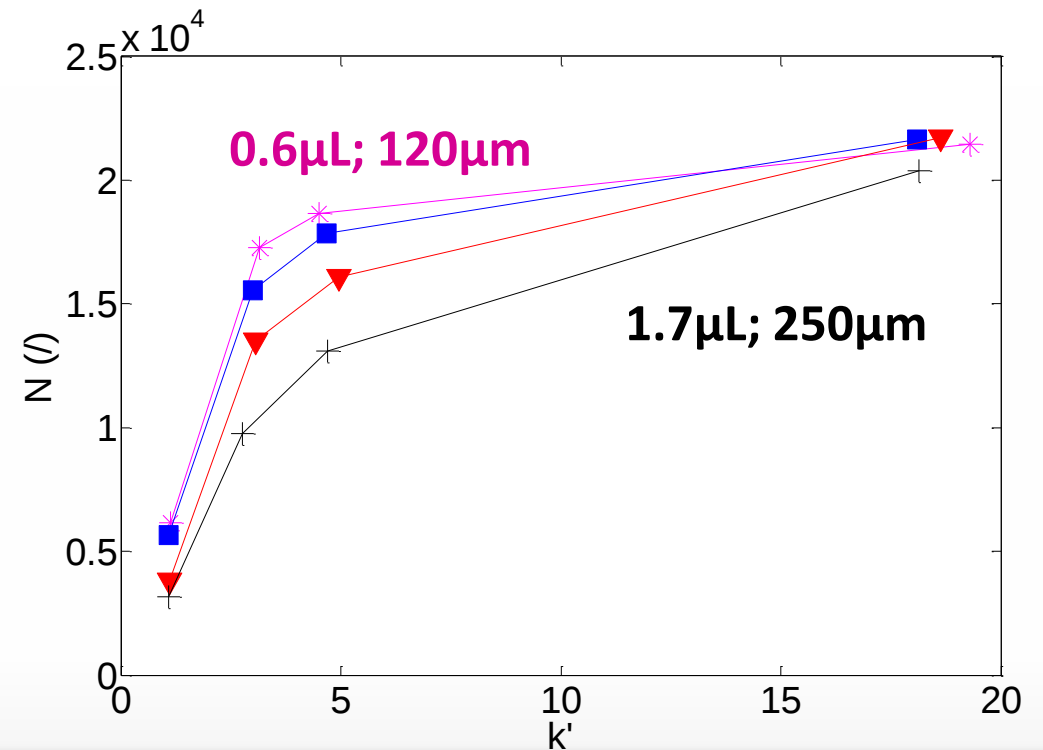
EXTRA-COLUMN BAND BROADENING

- Sources of extra-column dispersion in SFC: **tubing**
 - Sample solvent EtOH/IPA/hexane: 10/5/85, $V_{inj} = 0.8\mu\text{L}$
 - $P_{back} = 130$ bar, $2.1 \times 100\text{mm}$ $1.8\mu\text{m}$, $F = 1\text{ml/min}$, 8 V% MeOH
 - Tubing
 - Length (50cm)
 - Inner diameter variable
 - **250 μm**
 - **170 μm**



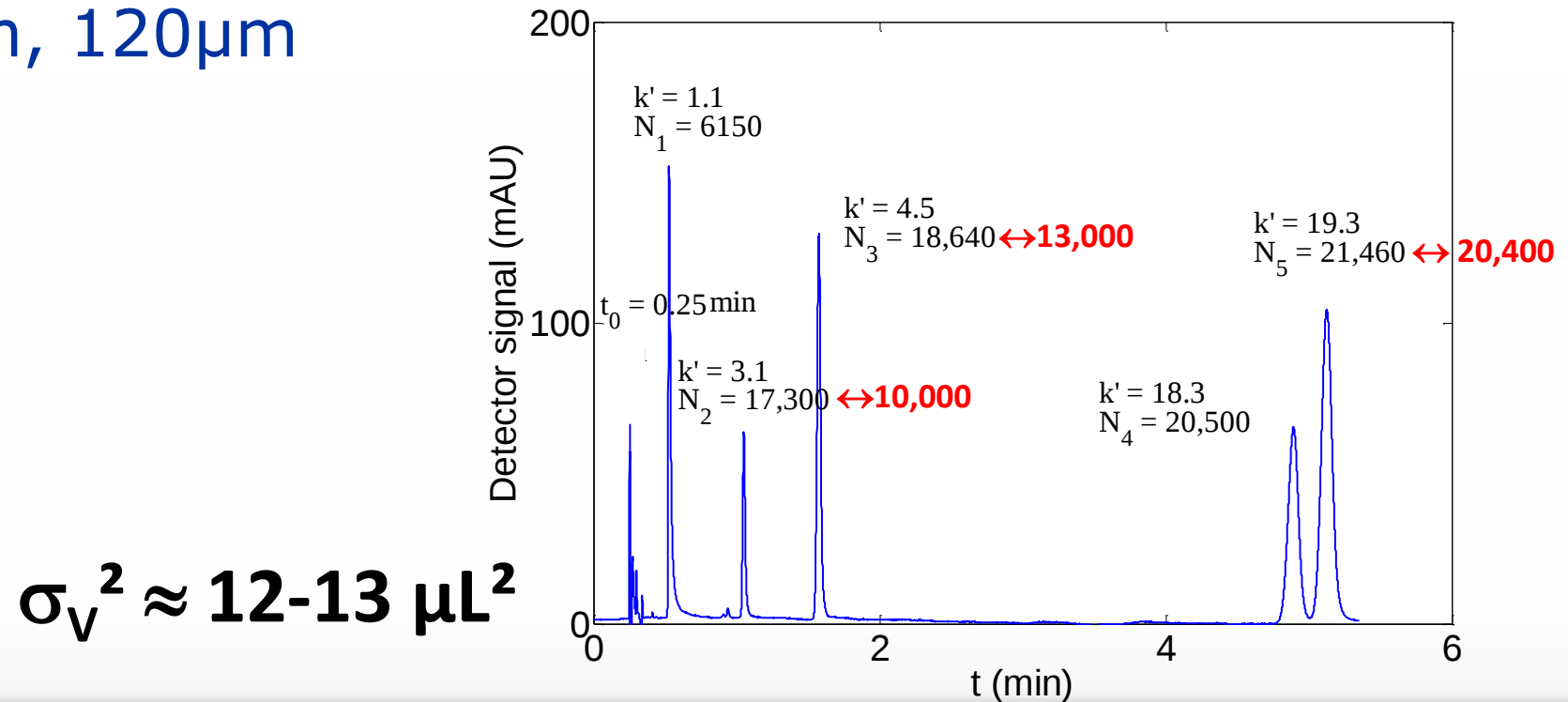
EXTRA-COLUMN BAND BROADENING

- Sources of extra-column dispersion in SFC: **tubing**
 - Sample solvent EtOH/IPA/hexane: 10/5/85, $V_{inj} = 0.8\mu\text{L}$
 - $P_{back} = 130$ bar, $2.1 \times 100\text{mm}$ $1.8\mu\text{m}$, $F=1\text{ml/min}$, 8 V% MeOH
 - Tubing
 - Length (50cm)
 - Inner diameter variable
 - **250 μm**
 - **170 μm**
 - **120 μm**



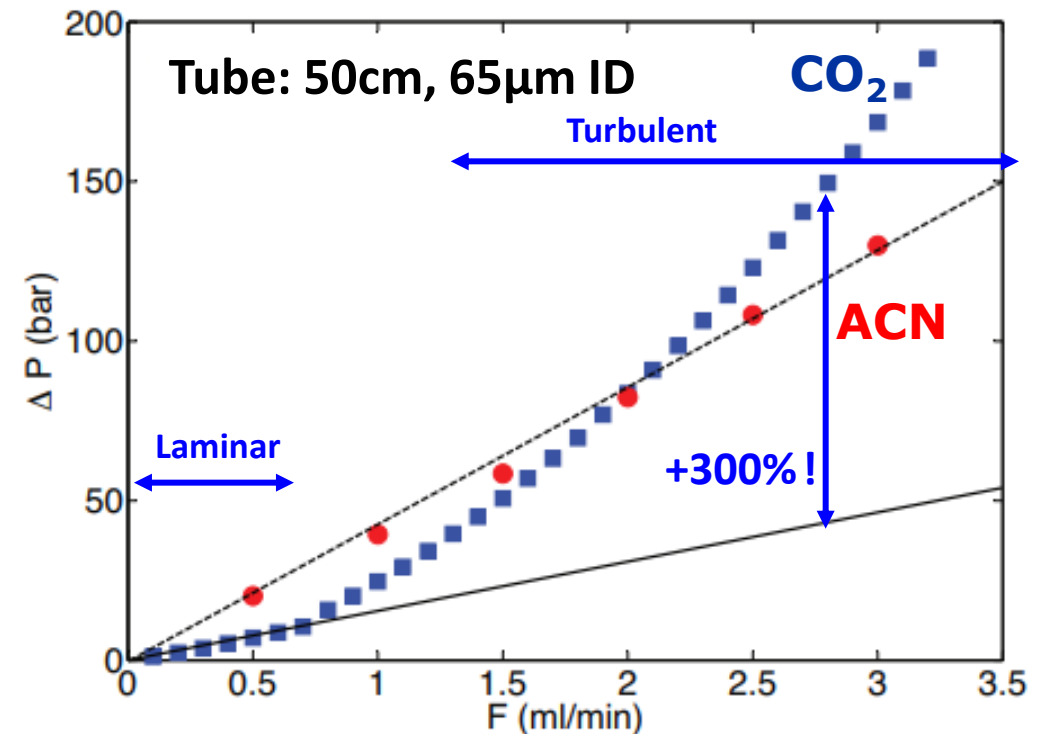
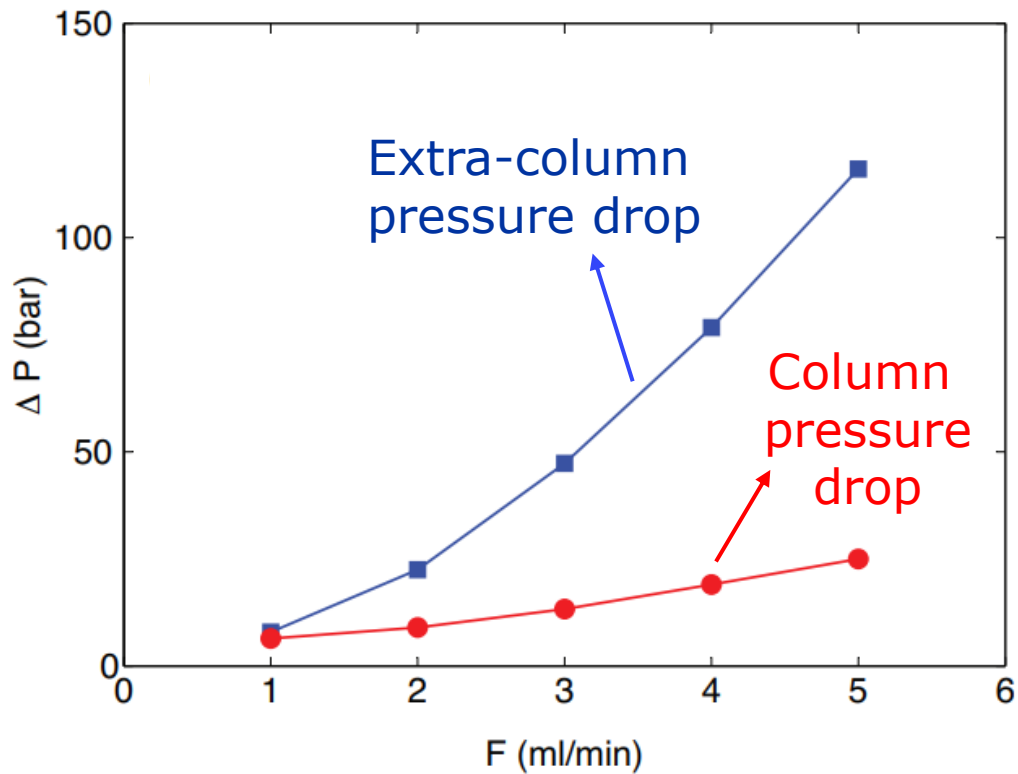
EXTRA-COLUMN BAND BROADENING

- Optimized system for minimal extra-column dispersion
 - Sample solvent EtOH/IPA/hexane: 10/5/85, $V_{inj} = 0.8\mu\text{L}$
 - $P_{back} = 130$ bar, $2.1 \times 100\text{mm}$ $1.8\mu\text{m}$, $F = 1\text{ml/min}$, 8 V% MeOH
 - Tubing 50cm, $120\mu\text{m}$



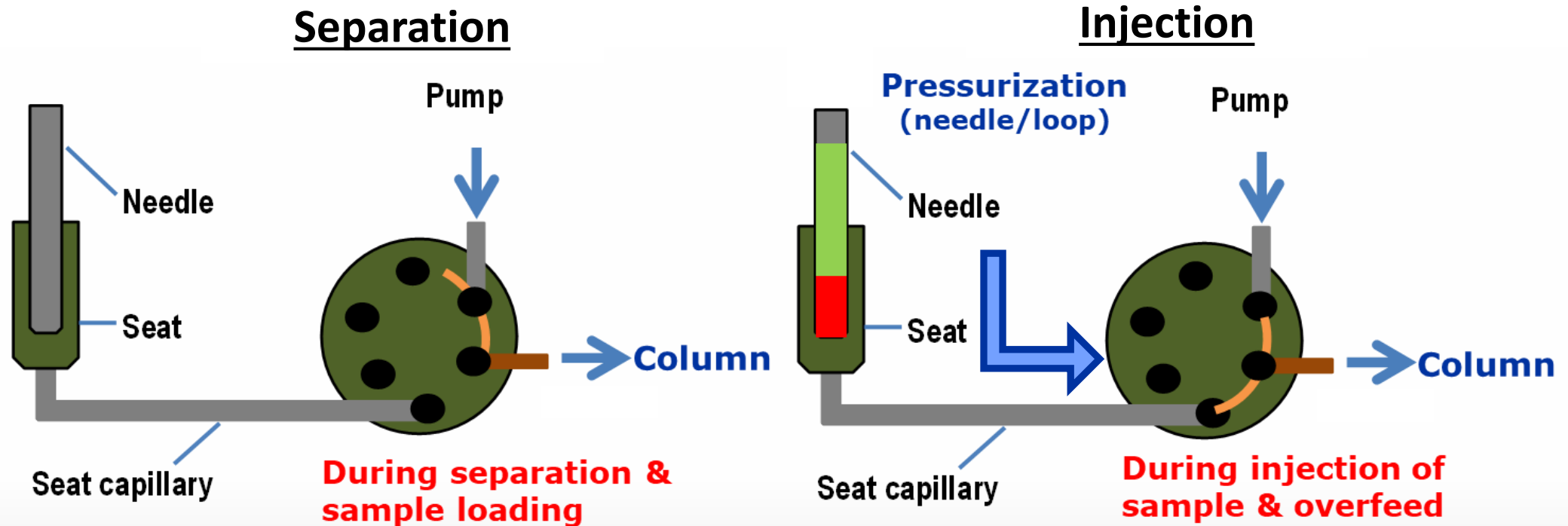
EXTRA-COLUMN PRESSURE

- Watch out for narrow ID tubing in SFC at high flow rate!
- 4.6 mm ID column (10% MeOH) and 120 μ m tubing in system



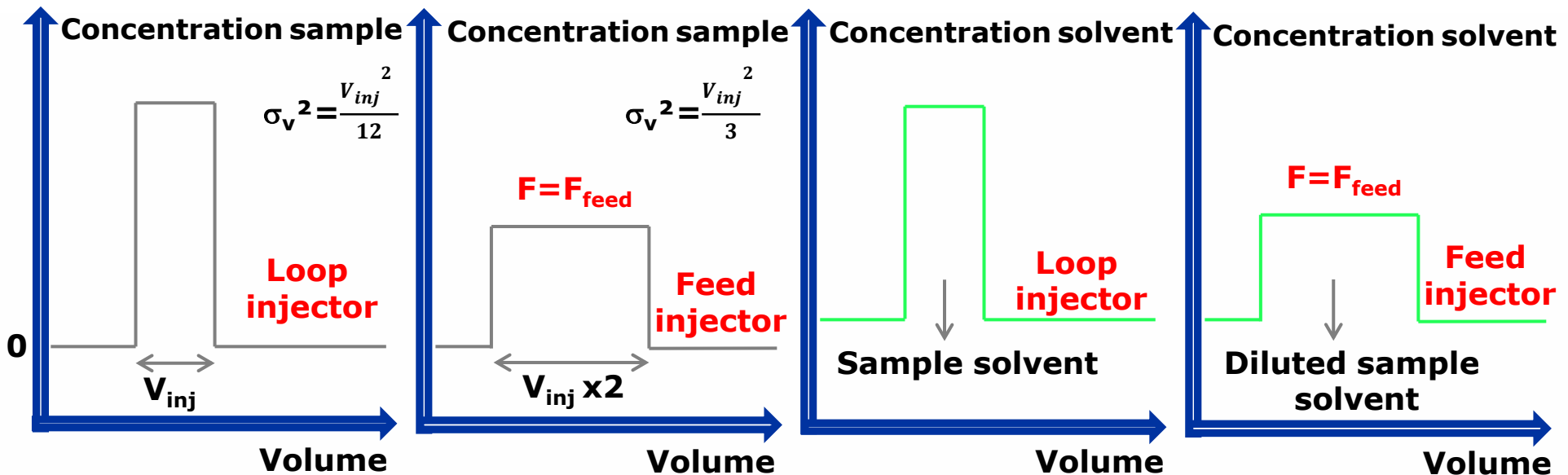
INJECTION/SAMPLE INTRODUCTION

- Feed injector: dilute sample with mobile phase
- Injection flow rate can be varied (max. 1 ml/min)
- **Overfeed volume** needed to fully inject loaded **sample volume**



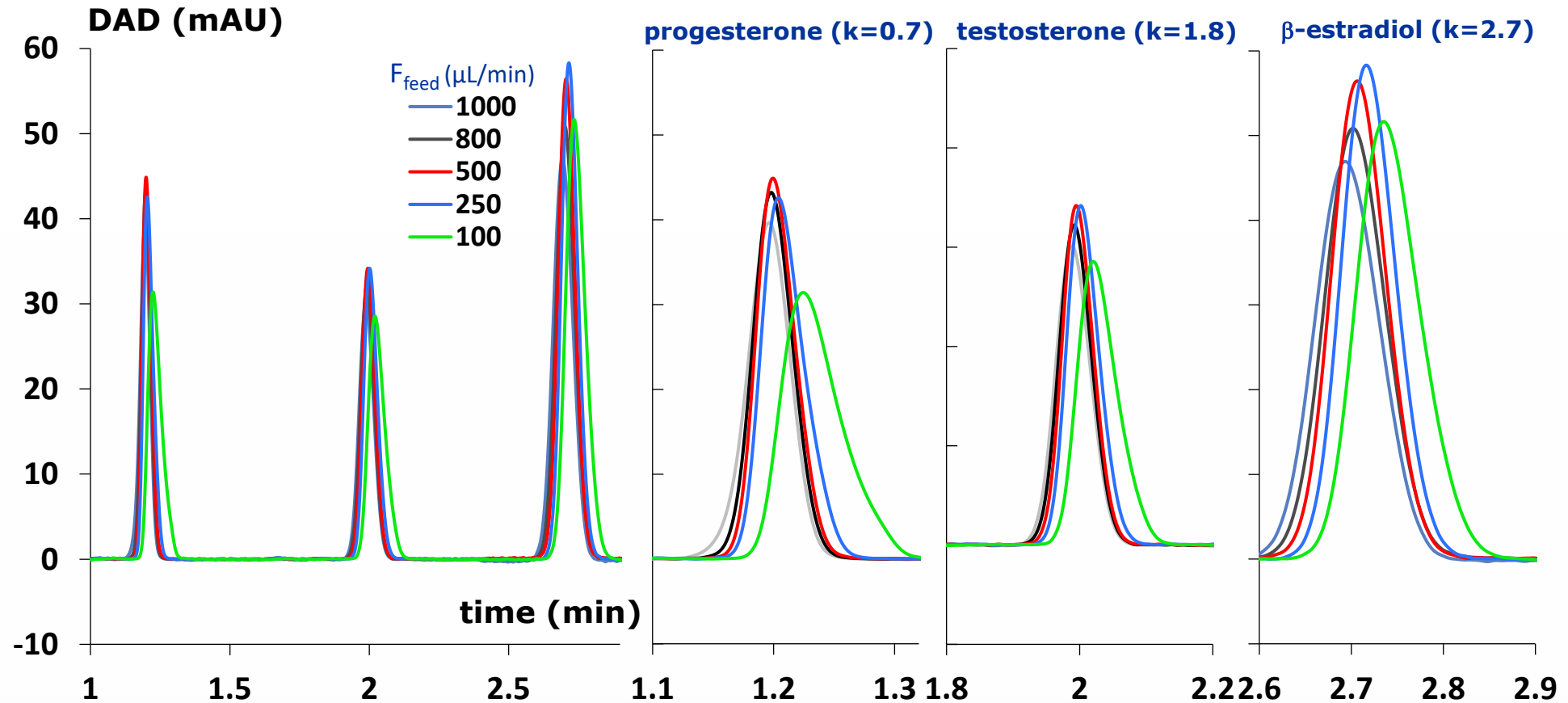
INJECTION/SAMPLE INTRODUCTION

- Feed injector: dilute sample with mobile phase
- Injected sample plug increases in volume $\sim 1 + F/F_{\text{feed}}$
- Sample solvent is diluted with mobile phase ($\sim$ mainly CO_2)



INJECTION/SAMPLE INTRODUCTION

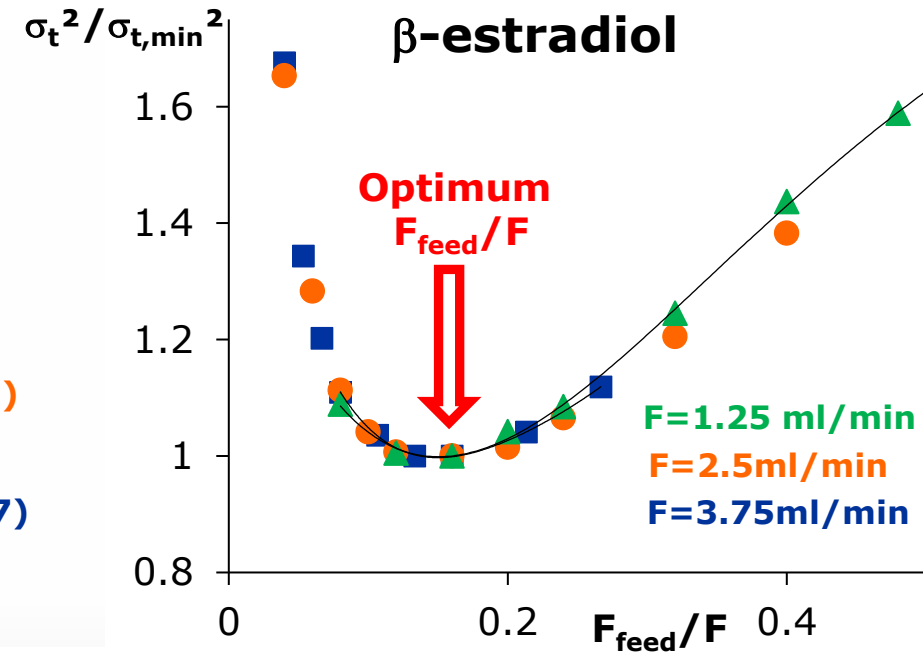
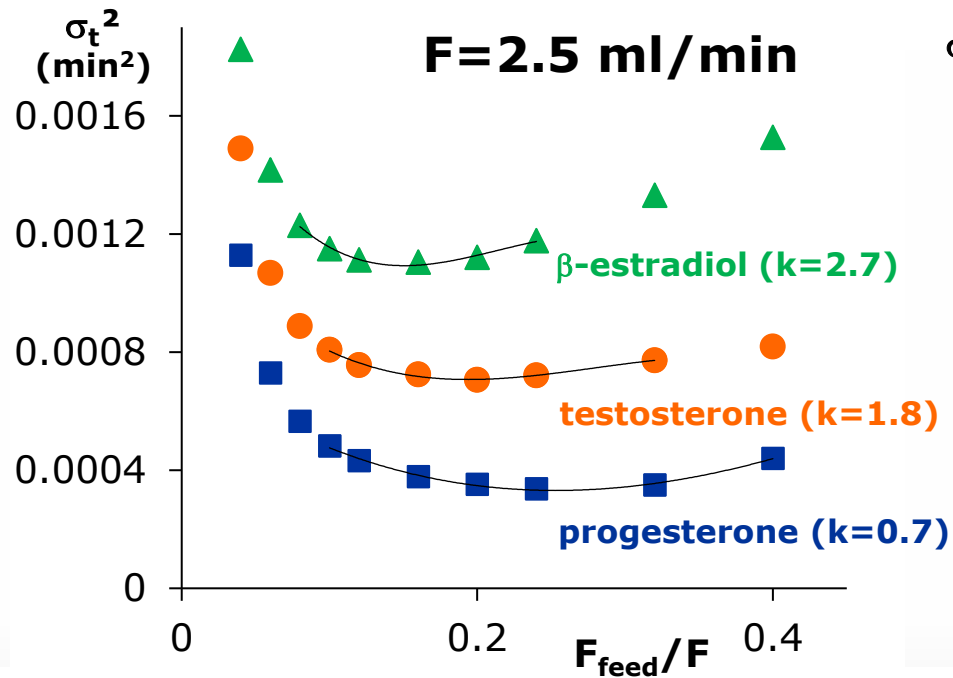
- Feed injector: effect of feed flow rate F_{feed} for $F = 2.5$ ml/min



Agilent Zorbax RX-SIL, 4.6 x 150mm 5 μm , 12% MeOH

INJECTION/SAMPLE INTRODUCTION

- Optimal feed flow rate F_{feed} found for strong dilution (3-6x)
- Optimal ratio F_{feed}/F independent on flow rate F
- Stronger dilution for solutes with larger dependency of k on ϕ



$V_{\text{inj}} = 2.5 \mu\text{L}$
 $V_{\text{ov}} = 4.0 \mu\text{L}$

CONCLUSIONS

- CO₂-based mobile phases exhibit interesting properties but are often overstated for modern conditions and applications
- Kinetic separation performance of modern SFC instruments is similar to UHPLC
- Need for backpressure and lower maximum pump pressure decreases potential gains from low viscosity mobile phase and application of UC-gradients
- Extra-column band broadening can still be significantly improved for SFC to fully exploit advantages for small superficially porous particles and narrow ID columns

HPLC 2025 BRUGES

BELGIUM

June 15-19, 2025

<https://hplc2025-bruges.org>

Top-level science amid
UNESCO world heritage

Strong focus on young scientists &
industry research



Registrations open: Dec. 9th, 2024
Oral abstract deadline: Jan. 15th, 2025